Industrial motivation



Steam generator in a power plant

S. C. Schultz. Steam, Its Generation and Use, 40th ed. Babcock & Wilcox Company, 1992

Industrial motivation

Important processes

- gas flow in the large scale burners
- combustion processes described by physical principles (burnout measured data)
- NOx chemistry
- energy release and transfer to water piping
- co-firing simultaneous combustion of biofuel



Measurement points in the burner

Geometry



Combustion chamber geometry

Mass conservation

Total-mass balance and chemical components balance laws

$$\begin{aligned} \frac{\partial \rho}{\partial t} + \frac{\partial (\rho v_i)}{\partial x_i} &= 0\\ \frac{\partial}{\partial t} (\rho Y_*) + \frac{\partial}{\partial x_i} (\rho Y_* v_i) &= \frac{\partial}{\partial x_i} \left(-\frac{\mu_T}{\mathrm{Sc}_t} \frac{\partial Y_*}{\partial x_i} \right) + \omega_* \end{aligned}$$

where * substitutes O_2, N_2, NO, HCN, NH_3, H_2O and CO_2

Char, volatiles and coal particle balance laws

$$\begin{aligned} \frac{\partial \rho_{\text{char}}}{\partial t} + \frac{\partial (\rho_{\text{char}} v_i)}{\partial x_i} &= R_{\text{char}} \\ \frac{\partial \rho_{\text{vol}}}{\partial t} + \frac{\partial (\rho_{\text{vol}} v_i)}{\partial x_i} &= R_{\text{vol}} \\ \frac{\partial n}{\partial t} + \frac{\partial (nv_i)}{\partial x_i} &= 0 \end{aligned}$$

Flow and heat transfer

Momentum and energy balance laws

$$\frac{\partial}{\partial t}(\rho v_i) + \frac{\partial}{\partial x_i}(p + \rho v_i^2) = \frac{\partial}{\partial x_j}\left(\mu \frac{\partial v_i}{\partial x_j}\right) + \frac{1}{3}\frac{\partial}{\partial x_j}\left(\mu \frac{\partial v_j}{\partial x_i}\right) - \frac{2}{3}\frac{\partial}{\partial x_i}(\rho k) + \rho g_i$$

$$c_p \left[\frac{\partial}{\partial t}(\rho T) + \frac{\partial}{\partial x_i}(\rho T v_i)\right] = -R_{char}h_{char} - R_{vol}h_{vol} - \nabla(\mathbf{q}_c + \mathbf{q}_r) + \frac{\partial}{\partial x_j}\left[\left(\mu_L + \frac{\mu_T}{\sigma_k}\right)\frac{\partial k}{\partial x_j}\right]$$

 $k-\varepsilon$ model for turbulence

$$\frac{\partial}{\partial t}(\rho k) + \frac{\partial}{\partial x_i}(\rho k v_i) = \frac{\partial}{\partial x_j} \left[\left(\mu_L + \frac{\mu_T}{\sigma_k} \right) \frac{\partial k}{\partial x_j} \right] + G_k - G_b - Y_m - \rho \varepsilon$$

$$\frac{\partial}{\partial t}(\rho \varepsilon) + \frac{\partial}{\partial x_i}(\rho \varepsilon v_i) = \frac{\partial}{\partial x_j} \left[\left(\mu_L + \frac{\mu_T}{\sigma_\varepsilon} \right) \frac{\partial \varepsilon}{\partial x_j} \right] + C_{1\varepsilon} \frac{\varepsilon}{k} (G_k + C_{3\varepsilon} G_b) - C_{2\varepsilon} \rho \frac{\varepsilon^2}{k}$$

$$p = \frac{\rho RT}{\bar{M}}, \quad \mu_T = \rho C_\mu \frac{k^2}{\varepsilon}, \quad \mu = \mu_L + \mu_T, \quad h_{char} + h_{vol} = LHV$$

$$G_k = \left(\frac{\partial v_1}{\partial x_2} + \frac{\partial v_2}{\partial x_1}\right)^2 + \frac{\partial v_1}{\partial x_1} \left[\frac{4}{3}\mu \frac{\partial v_1}{\partial x_1} - \frac{2}{3}\left(\rho k + \mu \frac{\partial v_2}{\partial x_2}\right)\right] + \frac{\partial v_2}{\partial x_2} \left[\frac{4}{3}\mu \frac{\partial v_2}{\partial x_2} - \frac{2}{3}\left(\rho k + \mu \frac{\partial v_1}{\partial x_1}\right)\right]$$

$$G_b = -g_i \frac{\mu}{\rho \Pr_t} \frac{\partial \rho}{\partial x_i}, \quad C_{3\varepsilon} = \tanh |\frac{v_2}{v_1}|, \quad Y_m = 2\rho\varepsilon M_t^2, \quad M_t = \sqrt{\frac{k}{a^2}}, \quad a = \sqrt{\gamma RT}$$

Chemistry

Simulation results

Case	Air distribution %				Fuel distribution %				Excess air coefficient				NO	CO_{2}	
	B_1	B_2	B_3	B_4	B_1	B_2	B_3	B_4	B_1	B_2	B_3	B_4	ppm		
1	25	25	25	25	25	25	25	25	1.3	1.3	1.3	1.3	357	20%	1.9%
2	50	20	20	10	25	25	25	25	2.6	1.04	1.04	0.52	177	20%	1.9%
3	10	20	20	50	25	25	25	25	0.52	1.04	1.04	2.6	134	20%	2%
4	25	25	25	25	50	20	20	10	0.65	1.63	1.63	3.25	182	18%	4.5%

- Case 1 uniform air and coal distribution over 4 pairs of burners
- Case 2 decreasing air and uniform coal distribution over 4 pairs of burners (with consequent excess or missing air fraction in burners)
- Case 3 increasing air and uniform coal distribution over 4 pairs of burners (with consequent excess or missing air fraction in burners)
- Case 4 uniform air and decreasing coal distribution over 4 pairs of burners (with consequent excess or missing air fraction in burners)



Case 1: Profiles of temperature (top), mass fraction of NO (middle) and mass fraction of CO₂ (bottom)



Case 2: Profiles of temperature (top), mass fraction of NO (middle) and mass fraction of CO₂ (bottom)



Case 3: Profiles of temperature (top), mass fraction of NO (middle) and mass fraction of CO₂ (bottom)



Case 4: Profiles of temperature (top), mass fraction of NO (middle) and mass fraction of CO₂ (bottom)

Simulation results - uniform burner composition



Time evolution of energy release and wall transfer

Simulation results - uniform burner composition



Vertical distribution of key system variables at a given time

Simulation results - staging 10, 20, 20, 50% air x coal *t* [s] – Total heating value [MW] —— Heat transfer to walls [MW]

Time evolution of energy release and wall transfer

Simulation results - staging



Vertical distribution of key system variables at a given time

Simulation results - OFA



Time evolution of energy release and wall transfer

Simulation results - OFA



Vertical distribution of key system variables at a given time